

TM-1611

# Design Note of a 10,000 Amp 2 MJoules Dump Resistor for the Magnet Test Facility

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#### 1. SUMMARY

This report contains the design notes of a 2 MJoules 10,000A, 1000V, dump resistor, with taps from 25 mOhms to 300 mOhms maximum. The resistor is forced air-cooled and can handle continuously one 2 MJ dump every 5 minutes at all taps. The resistor is made from 304 stainless steel bars and is mounted in a 90"H x 24"W x 20"D steel enclosure, with easy access to taps.

The upper resistance sections are made lighter to save material cost and weight. The total weight of the resistance element is 427 lbs.

The resistor is used to absorb the stored energy from cryogenic magnets during tests at the magnet test facility. Interlocks are provided for remote tap readout, dc over current and over temperature. A build-in current sensor and timing relay switch forced air-cooling on for 5 minutes, after a dump.

#### 2. AS BUILT DUMP RESISTOR PARAMETERS

nominal resistance taps at : 25, 50, 100, 150, 200, 250,

300 milliOhms<sup>1</sup>)

peak current : 10,000A

rms current : 500A at 100 mOhms

peak voltage : 1000V

power rating : one 2 MJ shot per 300 seconds

continuous at all taps

cooling : forced air for 5 min. after a

dump

temperature rise : 110°C peak, estimate

ambient temperature : 40°C maximum

insulation temp. class : 210°C

control power : 120 Vac, approx 5 A

enclosure size : 90"H x 36"W x 20"D, indoor

approx. weight : 1000 lbs.

(1) See test data for exact

values

#### 3. MTF DUMP RESISTOR DESIGN REQUIREMENTS

Design a dump resistor R<sub>D</sub> as follows:

- 1. 10,000A, 1000V maximum
- 2.  $300 \times 10^{-3} \Omega$  maximum
- 3. 6 taps at  $50x10^{-3}\Omega$  intervals
- 4. energy dissipation at each tap, 2 MJ
- 5. one 2 MJ dump/ $_{5 \text{ min}}$ , 6 dumps/ $_{hr}$
- 6. install remote tap setting readout

#### 4. GENERAL DESIGN APPROACH

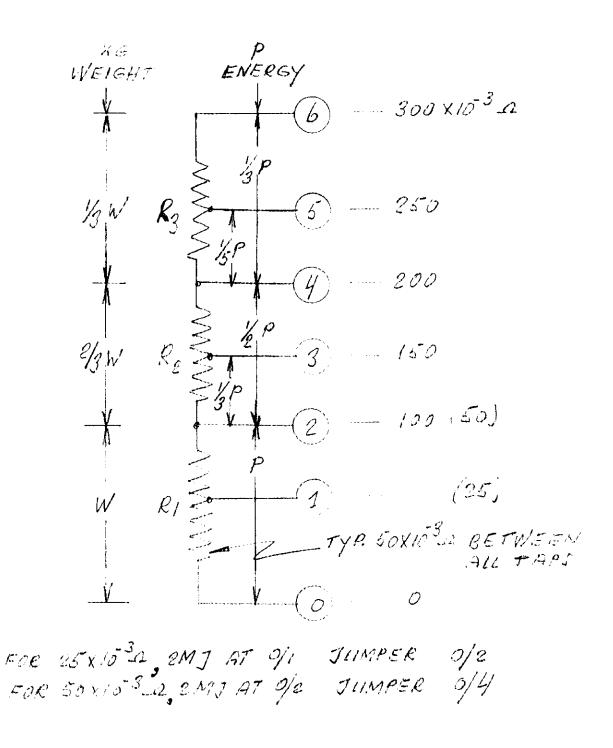
The temperature rise of the dump resistor steel is:

$$\Delta T = constant \times \frac{P}{W} \circ C$$

P is the instantaneous dump energy

W is the weight of the dump resistor steel

The dump resistor could be designed as shown in fig. 1.



Dump Resistor General Design Fig. 1

The dump resistor shown in fig. 1 is a reasonable approach. It consists of 3 sections of  $100 \times 10^{-3} \Omega$  each with a center tap. The weight of the sections changes for the higher values because the power dumped in those is a fraction of P. Making three resistor sections with different weights saves about 30% of the SS material cost. Each resistor section can be made from different size #304 stainless steel flat bars. These bars are commercially available in a large variety of sizes in 12 ft. length. Stainless steel type 304 has a reasonably high specific resistance and is therefore practical.

The amount of energy dumped in a kg of steel determines the temperature rise, assuming no losses to the ambient.

$$W = \frac{1/2LI^2}{C \Delta T} \text{ kg}$$

$$\frac{1}{2}$$
 L|2 = stored energy dumped in R<sub>D</sub>, in Joules

C = specific heat of  $R_D$  steel in Joules/ ${}^{\circ}_{Ckg}$ 

$$\Delta T$$
 = temp. rise in  ${}^{\circ}C$ 

No. 304 stainless steel has the following listed properties:

specific heat C  $_{\sim}$  500 Joules/ $^{\rm o}_{\rm C~kg}$ 

specific resistance at 
$$20 \text{ °C}$$
 =  $72 \times 10^{-6} \Omega \text{ cm}$ 

resistance temp. coeff. per  ${}^{\circ}C = 0.00094$ 

$$R_{90}^{\circ}C$$
 = 1.066  $R_{20}^{\circ}C$ 

specific weight = 0.00784 kg/cm3

A stainless steel bar, 1 ft. long with a crossection of 1 inch<sup>2</sup> has the following properties:

$$R/_{ft}$$
, 1 inch<sup>2</sup>, 20°C = 0.34x10<sup>-3</sup>  $\Omega$   
 $R/_{ft}$ , 1 inch<sup>2</sup>, 90°C = 0.362x10<sup>-3</sup>  $\Omega$   
weight/ft, 1 inch<sup>2</sup> = 3.4 lbs.

The temperature rise limit can be set by choosing the weight of the resistor steel large enough so that the temperature rise  $\Delta T$  for a 2 MJ dump does not exceed 50° C. Each individual 100 m $\Omega$  resistor section can be designed, based on the resistance, temperature rise and power dissipation requirements.

#### 5. **DUMP RESISTOR DESIGN**

#### 5.1 R1, 100 m $\Omega$ , 2 MJ Section

The amount of energy dumped in R<sub>1</sub> is at worst 2 MJ. Limiting the temperature rise to 50 °C yields:

$$W > \frac{2 \times 10^6}{500 \times 50} = 80 \text{ kg (176.4 lbs)}$$

Section  $R_1$  requires therefore a piece of stainless steel that has a resistance of  $100 \times 10^{-3} \Omega$  and weighs at least 176 lbs. Let the crossection of the stainless steel bars be S inch<sup>2</sup> with a total length of L ft. This choice has to satisfy:

and

$$\frac{0.34 \times 10^{-3}}{S}$$
 L <  $100 \times 10^{-3}$   $\Omega$  (resistance requirement)

Solve: 
$$S = 0.42 \text{ inch}^2$$

$$L = 123.5 \text{ ft.}$$

#### Choose:

$$R_{20}$$
oC = 0.725 x 10<sup>-3</sup>  $\Omega$ /ft

$$R_{90}$$
°C = 0.773 x  $10^{-3} \Omega/ft$ 

Need 138 ft for 100 x  $10^{-3} \Omega$  at  $20^{\circ}$ C

# Semi- Final Choice Section R<sub>1</sub>:

Total 132 ft, 
$$\frac{3}{16} \times 2\frac{1}{2}$$

$$R_{20} O_C = 95.7 \times 10^{-3} \Omega$$

$$R_{90} o_C = 102 \times 10^{-3} \Omega$$

$$W = 210.4 \text{ lbs } (114.3 \text{ kg})$$

$$\Delta T = 42^{\circ}C$$
 at 2 MJ

$$P = 9.5 \text{ kJ/lb}$$

The resistance of the purchased material needs to be checked so that the final cutting length can be calculated.

## 5.2 R<sub>2</sub>, 100 m $\Omega$ , 1.33 MJ Section

The amount of energy dumped in  $R_2$ , Section 2-3 (Fig.1) is  $\frac{1}{3}$  P maximum and  $\frac{1}{2}$  P maximum for total  $R_2$ . Assume for calculation purposes that the amount of energy dumped in  $R_2$  is at worst  $\frac{2}{3}$  x 2 MJ.

The weight of  $R_2 > 2/3 \times 176 = 117$  lbs

Thus:

$$3.4 \text{ SL}$$
 > 117 lbs   
  $\frac{0.34 \times 10^{-3}}{\text{S}} \text{ L}$  < 100 x 10<sup>-3</sup>  $\Omega$ 

Solve:  $S = 0.34 \text{ inch}^2$ 

L = 101.2 ft

Choose:

304SS,  $3/16 \times 2$ , 12 ft long flat bar. 1.275 lbs/ft, 0.375 inch<sup>2</sup>

 $R_{20}^{o}C = 0.9066 \times 10^{-3} \Omega/ft$ 

 $R_{900C} = 0.9665 \times 10^{-3} \Omega/ft$ 

need 110 ft for 100 x  $10^{-3} \Omega$  at  $20^{\circ}$ C

### Semi-Final Choice Section R2:

Buy 10 - 12 ft, cut to 11 ft

Total 110 ft, 3/16 x 2

$$R_{20}^{\circ}C = 99.7 \times 10^{-3} \Omega$$

$$P_{90}^{\circ}C = 106.3 \times 10^{-3} \Omega$$

$$W = 140.2 lbs$$

$$\Delta T = 42^{\circ}C \text{ at } 1.33 \text{ MJ}$$

$$P = 9.5 \text{ kJ/lb}$$

#### 5.3 R3, 100 m $\Omega$ , 0.67 MJ SECTION

The amount of energy dumped in  $R_3$ , Section 4-5 (Fig. 1) is 1/5 P maximum and 1/3 P maximum for total  $R_3$ . Assume for calculation purposes, that the amount of energy dumped in  $R_3$  is at worst 1/3 x 2 MJ.

The weight of  $R_3 > 1/3 \times 176 = 58.6$  lbs

Thus: 3.4 SL > 58.6 lbs 
$$\frac{0.34 \times 10^{-3}}{S} L < 100 \times 10^{-3}$$

Solve: 
$$S = 0.242 \text{ inch}^2$$
  
 $L = 71.1 \text{ ft}$ 

Choose:

304 SS,  $3/16 \times 1-1/2$ , 12 ft long flat bar

0.9563 lbs/ft, 0.28125 inch2

$$R_{20}^{\circ}C = 1.209 \times 10^{-3}\Omega/ft$$

$$R_{90}^{o}C = 1.289 \times 10^{-3} \Omega/ft$$

Need 82.7 ft for 100 x  $10^{-3} \Omega$  at 20°C

#### Semi-Final Choice Section R3:

Buy 8 - 12 ft, 3/16 x 1-1/2, cut to 10 ft

Total 80 ft, 3/16 x 1-1/2

$$R_{20}$$
°C = 96.7 x 10<sup>-3</sup>  $\Omega$ 

$$R_{90}$$
°C = 103.1 x 10<sup>-3</sup>  $\Omega$ 

$$W = 76.5 lbs$$

$$\Delta T = 38.4 \text{ °C at } 0.67 \text{ MJ}^{1}$$

$$P = 8.7 \text{ kJ/lb}$$

1) 
$$\Delta T = 45.9 \, ^{\circ}\text{C}$$
 for section 4-5 at 0.4 MJ

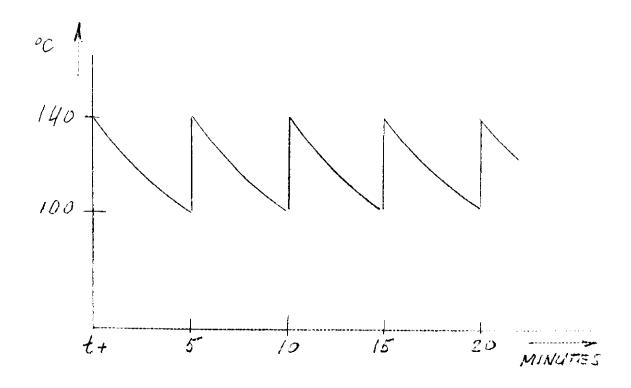
#### 6. COOLING CONSIDERATIONS FOR 2 M.I DUMPS

 $2 \text{ MJ/}_{5 \text{ min}} = 2000 \text{ kWsec/}_{300 \text{ sec}}$ 

The continuous equivalent power dissipation is 6.7 kW for one 2 MJ shot every 5 minutes. The  $R_1$  surface area is:  $12x11x12x5\frac{3}{8} = 8514$  inch<sup>2</sup>.

The power dissipation for  $R_1$  is approximately 0.78 watt/<sub>inch</sub>2.

Copper bars in free still air give  $\Delta T = 65^{\circ}$ C rise at ~0.5 watt/<sub>inch</sub>2. Forced air-cooling at ~200 ft/<sub>min</sub> reduces the thermal impedance by a factor ~2. With fans installed, the dump resistor temperature fluctuates approximately as shown in fig. 2.



Estimated dump resistor operating temperature with continuous 2 MJ dumps at 5 minute intervals.

Fig. 2

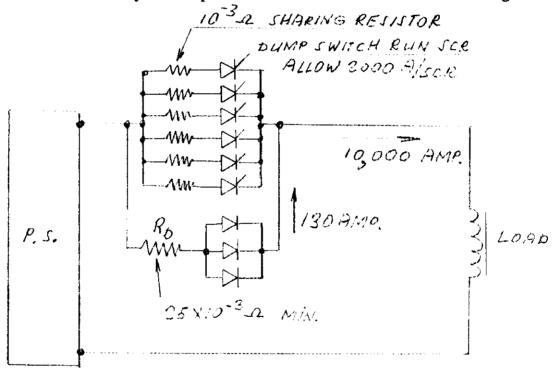
Choose: 1 - insulation: class 210°C for the resistor support spacers.

2 - fans on for 5 minutes after dump

3 - R<sub>D</sub> thermal intlk. ~120°C klixon.

#### 7. DUMP RESISTOR RUNNING LOSSES AND INTERLOCKS

The dump resistor is in parallel with the run SCR's of the dump switch and will carry some part of the dc current as shown in fig 3.



Basic electrical power diagram indicating operating current flow.

Fig. 3

The maximum running losses occur with the  $25x10^{-3}\Omega$  tap connection for  $R_D$ .

Max  $V_{RD} = 2000 \times 10^{-3} + V_{SCR} = 3.3 \text{ Volt}$ (Maximum run SCR and sharing resistor voltage drop)

$$I_{RD} = \frac{3.3}{25 \times 10^{-3}} = 130$$
 A normal running at 25 m $\Omega$  tap.

 $R_D$  running loss = 435 Watt max.

 $R_D R1 \text{ surface} = 8500 \text{ inch}^2$ 

 $R_D$  running power dissipation = 0.05 Watt/<sub>inch</sub><sup>2</sup> max.

The estimated worst  $\Delta T$  is approximately 15°C running.

A run SCR's turn-on (gating) failure can result in excessive dc current through R<sub>D</sub>. In that case R<sub>D</sub> will heat up and 120°C klixons at R<sub>D</sub> will trip the power supply.

A dc current sensor has also been installed at the power terminals of the dump resistor. It trips at about 300 Adc and prevents operation with large dc currents through the dump resistor or the dump resistor power cables. Large dc currents will occur with bolted shorts at the tap board or with run SCR gating failures.

The dc current sensor CS is simply a proximity switch (reed switch) mounted in the vicinity of the dump resistor power terminal bus. The contacts of a proximity switch will close as a result of the magnetic field created by the current flowing through the bus close to the switch.

It is an elegant solution, because it requires no control power and the contacts can be used directly in a 120 Vac control circuit. A similar current sensor starts the cooling fans after a dump.

The dump resistor is equipped with a "valid tap" interlock. It is possible to connect the tap links for a wrong combination. Interlocks at the taps keep the power supply off as a result of wrong tap connections. Remote tap position readout and interlock contacts have been provided. These interlock contacts must be used to prevent high operating currents when high resistance tap settings exist. Destructive high dump voltages, in excess of 1000V, will occur if a combination of high operating currents and high dump resistor values are permitted.

Drawing #ATV060489MTF shows the interlocks.

#### WARNING

Bolted shorts should not be installed at the dump resistor. A 10,000A rated shorting strap must be installed at the power connections to the dump switch if  $R_D=0\ \Omega$  is required for tests.

#### 8.0 DUMP RESISTOR CABLE SIZE

The dump resistor sees 2 MJ every 300 sec. The highest current values occur at the 25 x  $10^{-3}\Omega$  tap setting, which yields the highest rms current I in the  $R_D$  power cables.

$$I^2x25x10^{-3}x300 = 2000.000$$

$$I = 516 \text{ Amp}.$$

Thus the equivalent rms value of continuous dumps every 5 minutes would be 516 Amp. Connect the dump resistor with  $3 \times 2/0$  cables in parallel

Cable Ampacity 3x185 = 555 Amp. for  $90^{\circ}$ C cable insulation.

Cable O.D. ~0.54"

# 9. MATERIAL RESISTANCE MEASUREMENT

#### **DUMP RESISTOR S. STEEL TEST, OF MATERIAL RECEIVED**

| MATERIAL<br>SS#304                             | CALCULATED<br>R <sub>20</sub> ° <sub>C</sub> / <sub>ft</sub><br>x10 <sup>-3</sup> Ω | MEASURED $R_{20}{}^{\circ}_{\text{C}/\text{ft}}$ $x_{10}{}^{-3}_{\Omega}$ 1) |
|--|---|--|
| $3/16 \times 2\frac{1}{2}$                     | 0.725   | 0.6615*  |
| $3/16 \times 2$<br>$3/16 \times 1 \frac{1}{2}$ | 0.9066<br>1.209   | 0.9117*<br>1.2271*   |

<sup>\*</sup>adjusted for 20°C, material was tested at 32°C.

1 - Method: Put 5A through 8 ft. length, measure volt. drop in mV and divide by 40 for  $m\Omega/f_t$ .

NOTE: Published 304 resistance temp coeff = 0.00094 per °C.

#### **CALCULATE:**

$$3/16 \times 2-1/2 \quad R/_{\rm ft} \text{ at } 100^{\rm o}{\rm C} = 0.7112 \quad m\Omega$$
  
 $3/16 \times 2 \quad " = 0.9803 \quad m\Omega$   
 $3/16 \times 1-1/2 \quad " = 1.3194 \quad m\Omega$ 

# 10. FINAL CHOICE OF BAR LENGTH FOR DUMP RESISTOR SECTIONS

Calculate the final bar length of the dump resistor sections from the test data of para. 9. Make  $R_D$  300 m $\Omega$  at 100°C.

1. 
$$R_1 \text{ length } \frac{100}{0.7112} = 140.6 \text{ ft.}$$

2. 
$$R_2 \text{ length } \frac{100}{0.9803} = 102 \text{ ft.}$$

3. 
$$R_3$$
 length  $\frac{100}{1.3194}$  = 75.792 ft.

#### 11. DUMP RESISTOR ASSEMBLY PROCEDURE

This procedure yields 50 m $\Omega$  dump resistor sections at 100°C, based on the measured resistance of the 304 SS bars received.

Cut the stainless steel bars to the following length:

Stack pcs per drw. #ATV050989MTF line up ends at 0', weld together, weld stops, install tap board and mount assembly to enclosure backplate.

Remove center clamp top channel, cut slots in lower insulator for klixons, install 2 layers kapton between klixons and resistor steel. Reassemble.

Put R<sub>D</sub> in enclosure.

Make 2-7/8 dia. hole in enclosure top for R<sub>D</sub> cables.

Install fans, wiring and control cable hole.

Hipot -2500 VDC 1 min, measure resistance at various taps.

#### 12. DUMP RESISTOR TEST DATA

Date of test: January 1990

| 1. | Measured resistance of stainless steel length between tap:  0 - 1  1 - 2  2 - 3  3 - 4  4 - 5 | *milliOhms at 20°C |  |
|----|---|--------------------|--|
|    | 0 - 1   | 44.70              |  |
|    | 1 - 2   | 45.19              |  |
|    | 2 - 3   | 44.18              |  |
|    | 3 - 4   | 44.11              |  |
|    | 4 - 5   | 45.42              |  |
|    | 5 - 6   | 45.28              |  |

<sup>\*</sup>Accuracy ±0.05%

# 2. Measured resistance at nominal tapsetting:

| Nominal tap<br>milliohms | Measured milliohms at |             |             |
|--------------------------|-----------------------|-------------|-------------|
|                          | *20°C                 | 1)<br>100°C | 1)<br>150°C |
|                          |                       |             |             |
| 25                       | 22.52                 | 24.21       | 25.05       |
| 50                       | 44.61                 | 47.96       | 49.62       |
| 100                      | 89.93                 | 96.69       | 100.02      |
| 150                      | 134.13                | 144.22      | 149.18      |
| 200                      | 178.80                | 192.25      | 198.86      |
| 250                      | 224.46                | 241.34      | 249.65      |
| 300                      | 269.73                | 290.01      | 300.00      |

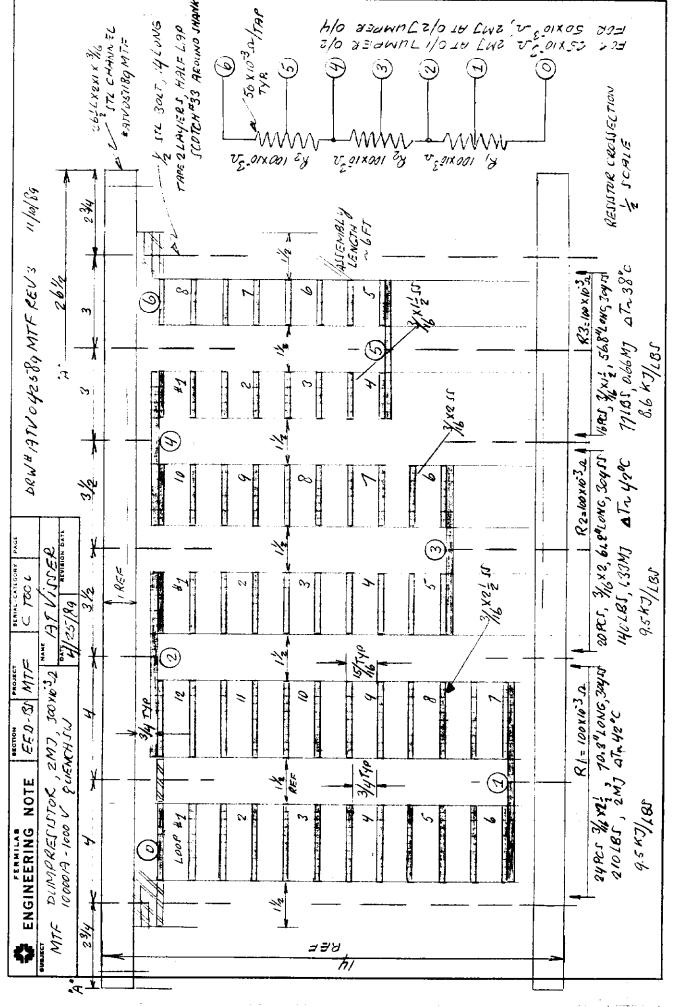
<sup>\*</sup>accuracy ±0.05%

1)calculated from 20°C

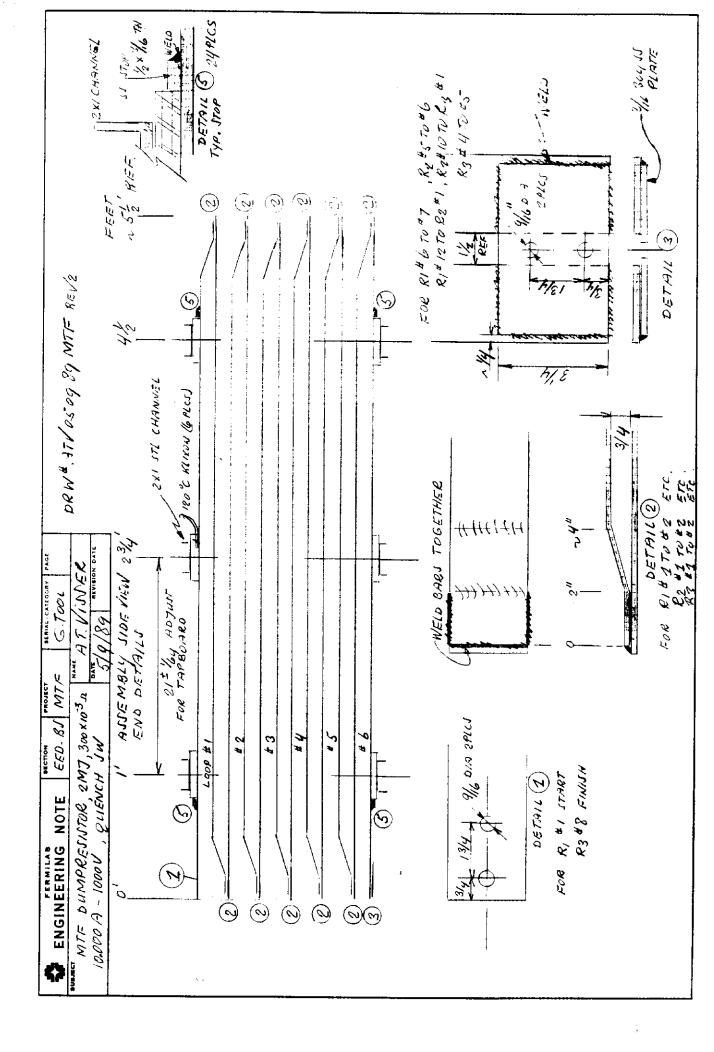
- 3. CS1 pickup 312 A, dropout 285 A CS2 pickup 284 A, dropout 280 A
- 4. High potential test 1 minute at 2500VDC >5000  $M\Omega$
- 5. All interlocks checked OK

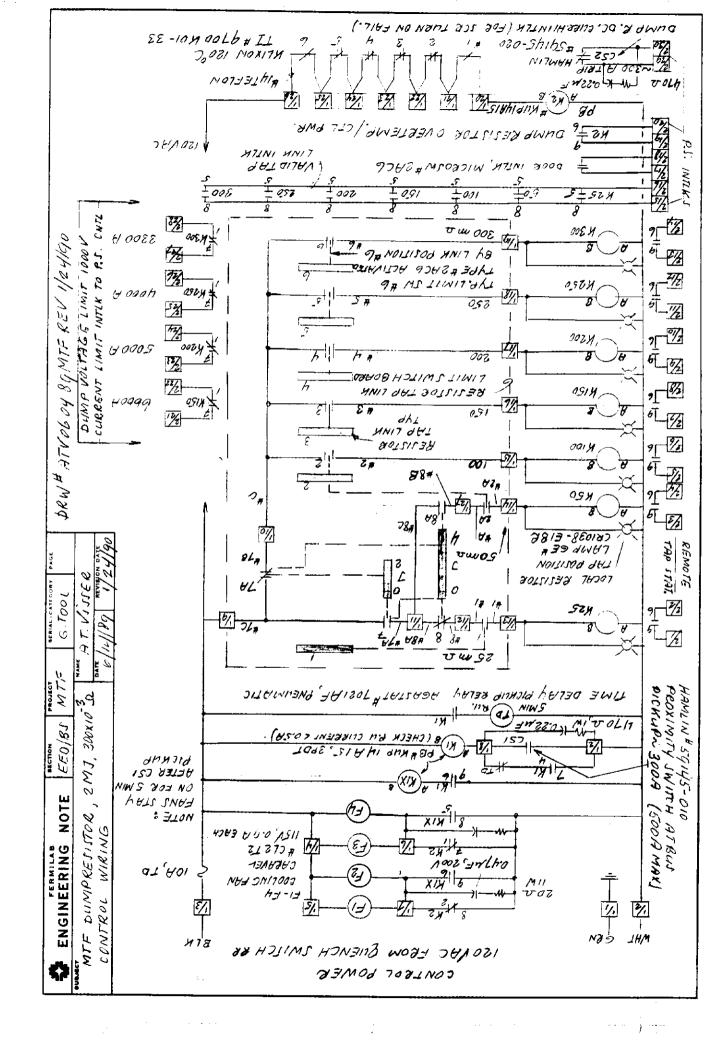
# 13. ACKNOWLEDGEMENTS

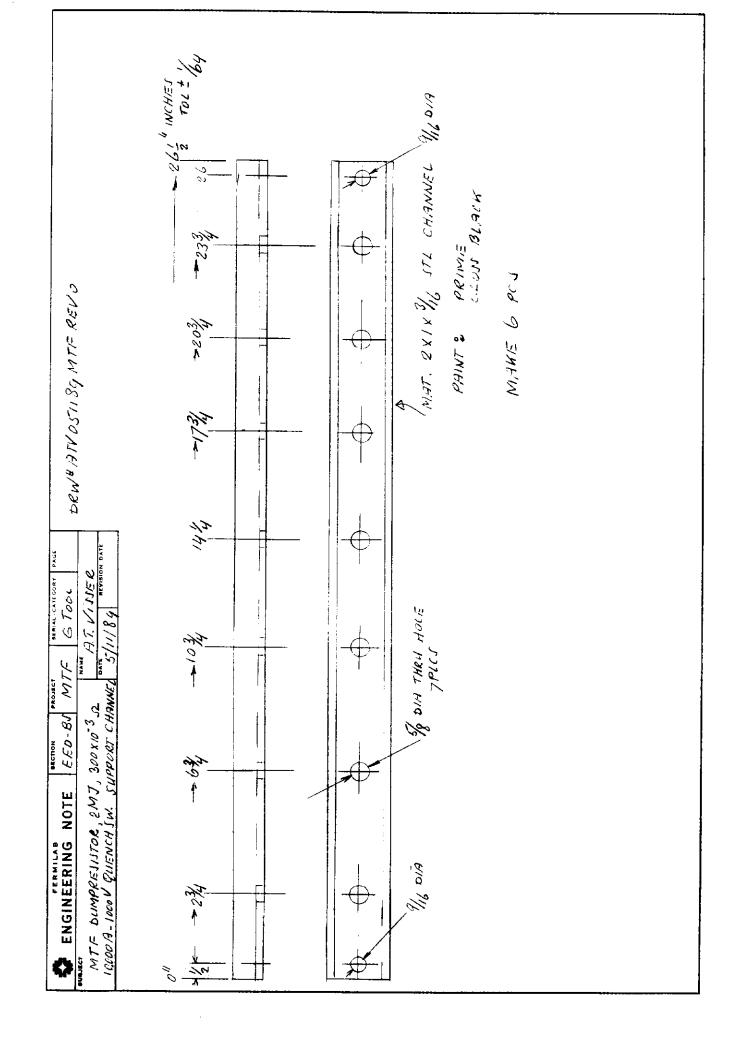
The resistor was assembled by EED personnel. Don Carpenter and Bob Oudt supervised the mechanical construction and Walt Jaskierny the electrical wiring and testing. I am grateful for their competent support.

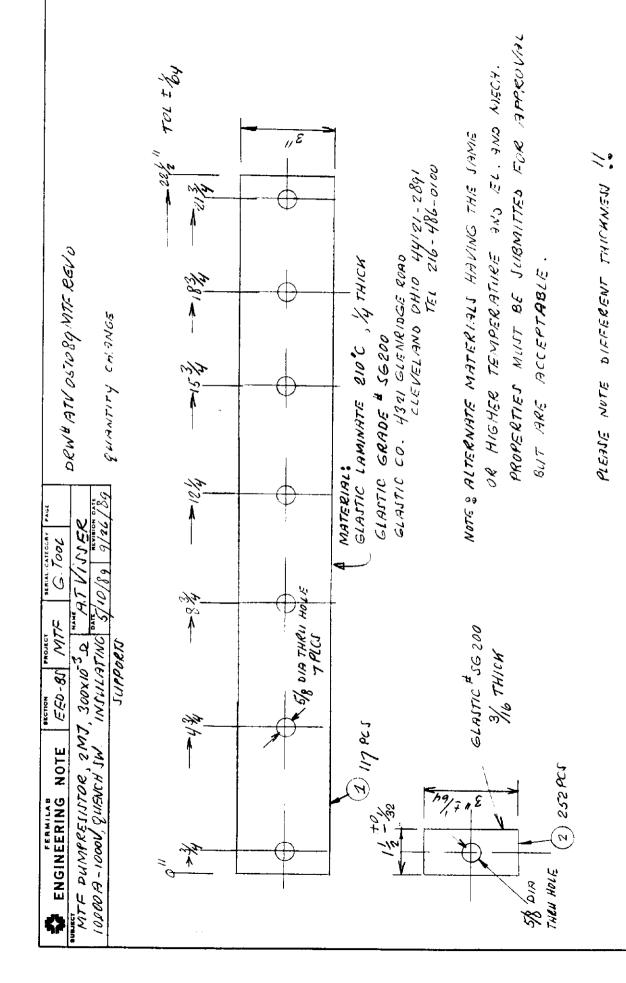


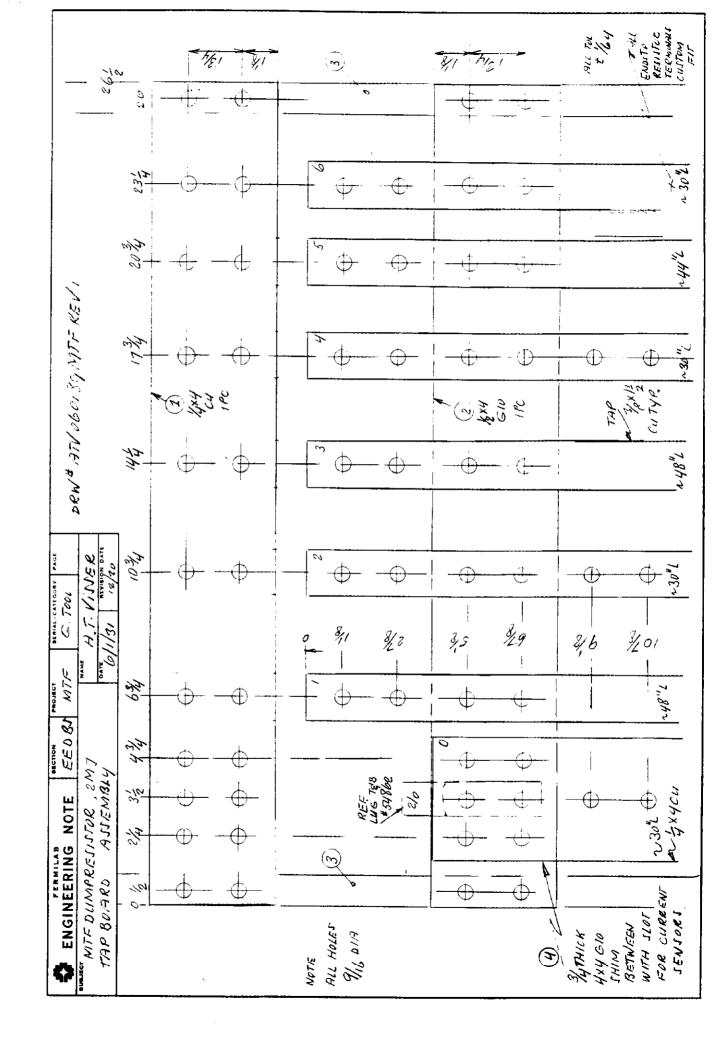
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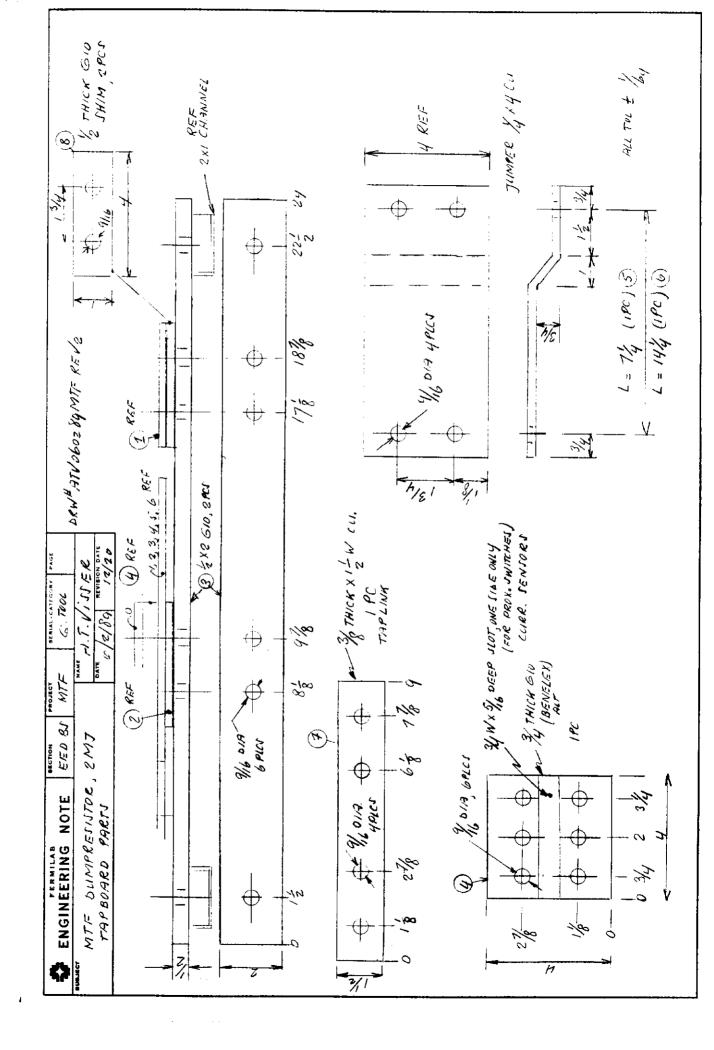


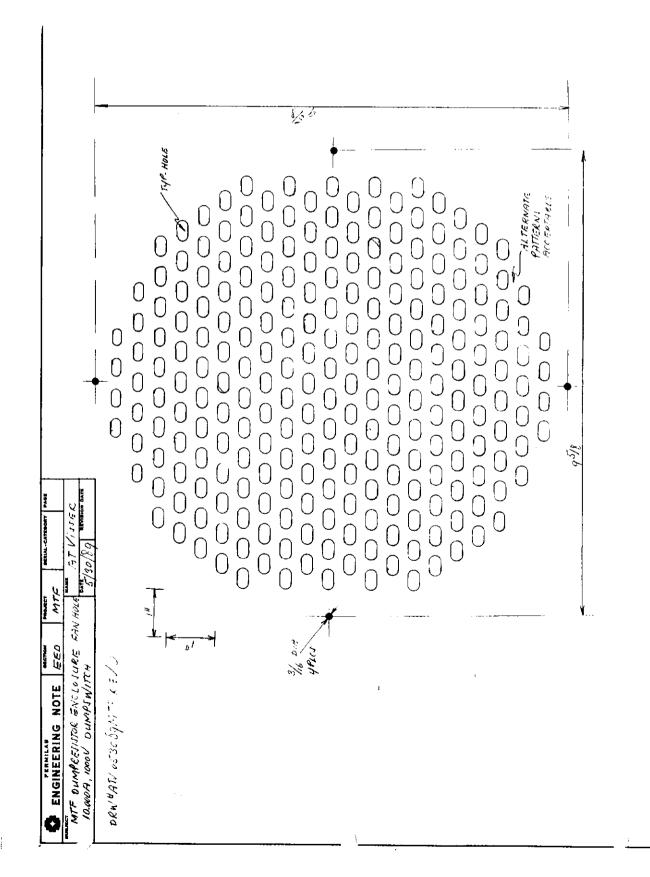




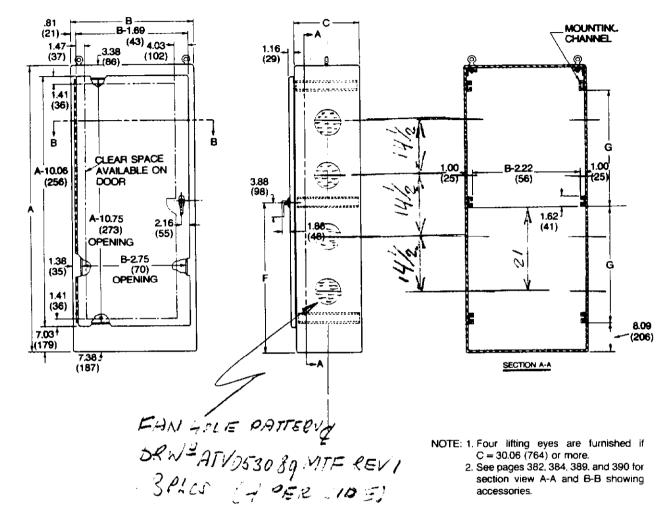








#### SINGLE DOOR SINGLE ACCESS ENCLOSURES



NOTE: 1. Four lifting eyes are furnished if C = 30.06 (764) or more.

2. See pages 382, 384, 389, and 390 for section view A-A and B-B showing accessories.

DUTSIDE PAINT - FINISH COAT DIARK BLUE

COLOR NUMBER 15180 IN FEDERAL STANDARD #5959 **Enclosure Size Enclosure Size** Enclosure G Catalog Number **AXBXC** G Catalog Number **AxBxC** 38.03 29.12 ± A-602418FS 60.06x24.06x18.06 32.03 23.12 § A-722424FS 72.06x24.06x24.06 (1830x611x611) (966) (740)(1526x611x459) (814)(587)72.06x30.06x24.06 38.03 29.12 29.12 § A-723024FS § A-722418FS 72.06x24.06x18.06 38.03 (966) (740)(1830x764x611) (1830x611x459) (966)(740)72.06x36.06x24.06 38.03 29.12 § A-723018FS 72 06x30.06x18.06 38.03 29.12 § A-723624FS (966)(740)(1830x916x611) (966)(740)(1830x764x459) 90.06x36.06x24.06 47.03 38.12 72.06x36.06x18.06 38.03 29.12 § A-903624FS § A-723618FS (2288x916x611) (968)(1195)(1830x916x459) (966)(740)29.12 72.06x36.06x30.06 38.03 § A-723630FS § A-902420FS 47.03 38.12 90.06x24.06x20.06 (1830x916x764) (966)(740)(968)(2288x611x510) (1195)38.03 29.12 72 06x36 06x36.06 A-903620FS 90.06x36.06x20.06 47.03 38,12 § A-723636FS (966)(740)(2288x916x510) (1195)(988) (1830x916x916) 47.03 38.12 t A-603624FS 60 06x36 06x24 06 32.03 § A-903636FS 90.06x36.06x36.06

23.12

(587)

Millimeter dimensions ( ) are for reference only; do not convert metric dimensions to inch.

(1526x916x611)

Certified by Canadian Standards Association. Specify CSA label when ordering. Certified by Canadian Standards Association. Specify CSA label when ordering. Consult factory for delivery.

(814)

Dew = 7+4053189 MTI= REVI

(968)

(1195)

(2288x916x916)